城市污泥堆肥温度的空间变异性研究

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关键词:空间变异性;静态垛;堆肥;城市污泥;温度;克里格插值

Spatial Variability of Temperature During the Sewage Sludge Composting Process

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Abstract: The studies of spatial variability had been undertaken during geology, agrology and ecology since 1980's, but the theory of spatial variability had not been used in the composting science. Composting temperature varied at different positions in the composting pile, which was the spatial variability of temperature, and it was a universal phenomenon during the composting process.

The composting temperature was high at some positions and low at other positions because of the temperature spatial variability. If the temperature was too high or too low, the process of eliminating pathogen or stabilization of organic matter was impeded. So it was necessary to know the spatial pattern of temperature in the pile, and know the location and ratio of composting material that had achieved the standard of land application.

The composting material that could not achieve the standard should be composted again. The quality of compost was improved when improving the composting technologies-such as adjusting the mixing ratio and the strategy of aeration-according to the temperature spatial pattern. The spatial variability of temperature was well expressed when analyzing and explaining the spatial data of temperature with the Geostatistics method.

The aims of this study were to analyze the temperature spatial variability in composing pile, and optimally interpolate the unmeasured temperature data depending on the measured data.

The aerated static pile was designed in a building with the one 6.0m×2.0m bay with cement floors and walls. Aeration boards were laid on the bottom of the bay. The pile contained sewage sludge (dry

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matter=19.3 percent) and bulking agent with the ratio of 1:1 by volume. A bulking agent layer on the aeration board dispersed air through the 1.0 m high mix layer. The pile was covered with a 20-cm insulating layer of recycled compost. There were two chambers built on the bottom of the bay and two aerating quantities, 0.79m³/(min • m³) and 2.03m³/(min • m³), were tested. The temperature sensors were inserted into the different designed positions of the pile to detect the temperatures on the two profiles with dimensions of 6.0m×1.0m. Using all available data of main nodes with the grids of 0.5m by 0.1m analyzed the temperature spatial structure. The detected temperature during the geometrical center of the pile was fed back to the computerized control system. A three-stage control algorithm controlled the damper duty cycle of the aerator. The primary composting process had been undertaken for 16 days. A computer installed with a automatic control software (Compsoft) logged temperatures of all positions and generated reports.

The semivariogram analysis was carried out to study the temperature spatial variability. The semivariogram of temperature increased gradually with the increasing of distance. When the distance was longer than α (correlation range), the semivariogram was invariable. The temperature changing during the composting process was decided by the determined variability and the randomicity variability, but the changing and distribution of temperatures during the field were usually decided by the determined variability.

The semivariogram function following to the 0° direction was different from that of the 90° direction, which showed that the temperature spatial variability held the characteristic of orientation. The different varying principles of temperature showed the semivariogram functions were not completely similar when the directions changed.

The temperature semivariogram functions of horizontal and vertical direction were simulated with the globosity model and the linearity model, respectively. The correlation ranges of profiles along the horizontal direction were 0.90 and 1.25m respectively and that following to the vertical direction were 0.75 and 1.00m respectively. So the temperature change in the pile was not completely unattached. It was important to study the correlation field of sampling spots and then decide the dimension of experimental area and the sampling locations.

The unmeasured composting temperature values were interpolated with the KRIGING method. The temperature isoline showed that the high temperature region located at the middle level, $0.4 \sim 0.6 \text{m}$, of the composting pile and the low temperature area lay in the substrate $0 \sim 0.4 \text{m}$. Estimated with the temperature isoline, the practical aerating quantity of moderate scale composting pile was under $0.79 \text{m}^3/\text{min} \cdot \text{m}^3$). So the KRIGING method can be used to study the temperature distribution in the composting science.

Key words: spatial variability; static pile; composting; sewage sludge; temperature; KRIGING method 文章编号:1000-0933(2002)06-0916-06 中图分类号:S141.6, X705 文献标识码:A

国外学者在 20 世纪 60 年代就提出了空间变异性的概念,经过近 40 年的努力,空间变异性理论已经取得长足的进展,研究方法从 Fisher 的经典统计分析过渡到 Matheron 提出的地统计学(Geostatistics),并将理论研究成果应用到实际当中 $[1^{-3}]$ 。 20 世纪 80 年代初期,国内学者逐步认识到,地统计学在土壤空间格局、植物群落空间变异等方面的研究上显示出经典统计学不可替代的优越性,于是空间变异性研究先后在地质学、土壤学、水科学、生态学等领域中的应用不断增多 $[4^{-7}]$,但是空间变异性理论在堆肥科学上运用仍未见报道。 万方数据

污泥好氧堆肥的堆体是一个复杂的生物反应系统,堆体内部各部分的物料均匀度、通气状况等性质存

在着差异,鼓风供氧控温过程、气温等外界因素对堆体不同位置的影响不尽相同,所以堆体各部分的温度存在较大差异^图,这就是所谓温度的空间变异性。这种情况在堆肥中是一种普遍现象。

堆体各部位温度的变化不均衡导致堆体温度的空间变异性,具体表现就是堆体内部某些部位温度高而某些部位的温度低。过高或过低的温度对于堆肥过程的高温灭菌过程和稳定化过程都不利[®],这就需要了解温度在堆体内部的空间格局,知晓达到处理标准的部分所处的位置及比例。这样就可以对未达标处理的物料进行回流处理,根据堆体温度空间格局改进工艺(混料比例、通风量、通风措施等),提高好氧堆肥的处理达标率。经典统计学由于其基本假设的限制,不能用于研究堆体温度的空间变异性,地统计学理论则提供了定量地描述和解释空间变化特性或空间自相关的方法,而且可以建立有关的空间预测模型并进行空间数据的插值和估计^{□®}。因此,借助于地统计学方法对堆肥温度空间数据进行有效地分析和解释,就可以准确表达堆体温度的空间变异性。

本研究的目的就是根据观测资料,分析温度的空间变化特性和参数间的空间关系,并对未测点的温度进行最优估值。这一研究对于了解堆体温度的空间格局,并将结果用于改进堆肥工艺具有重要意义。

1 材料与方法

试验采用北京方庄污水处理厂脱水污泥,含水率 80.7%,挥发性有机物含量为 49.2%。调理剂(型号 CTB)的含水率和饱和含水率为 2.68%、65.7% [11]。堆肥池大小为 $6.0m\times2.0m\times1.1m$,底部为布气板。堆肥池底部有两个风室,分别采用 $0.79m^3/(\text{min} \cdot \text{m}^3)$ 、 $2.03m^3/(\text{min} \cdot \text{m}^3)$ 两种通风量。试验装置见相关文献 [12]。采用中国科学院地理科学与资源研究所环境修复室研制的温度传感器、温度变送器、CTB 堆肥自动测控系统及 Compsoft 软件对堆肥过程进行控制。

试验时间为 2000 年 8 月 1 日 \sim 2000 年 8 月 11 日,混料比例为 1:1 (体积比,污泥:调理剂),将堆肥物料充分混匀后上堆。沿着堆肥池长度方向设定 2 个纵剖面(剖面 I 、I),对应 $0.79 m^3/(min \cdot m^3)$ 、 $2.03 m^3/(min \cdot m^3)$ 两种通风量,剖面上的温度状况代表堆体温度的空间格局。每个纵剖面的面积为 $6.0 m \times 1.0 m$,按 $0.5 m \times 0.1 m$ 布设网格,共设 53 个测点,测定时间 8 月 4 日。利用 SURFER 软件对数据进行作图。

2 结果与讨论

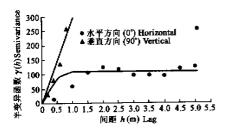
2.1 堆体温度的空间变异结构

温度是一个空间位置变化的区域化变量,假设其在所研究的区域里满足本征假设,则其半变异函数 γ (h)为:

$$\gamma(h) = \left(\frac{1}{2N}\right) \sum_{i=1}^{N} \left[Z(x_i) - Z(x_i + h) \right]^2 \tag{1}$$

式中,h 为分隔两个观测点的距离,即为滞后距,N 为被,h 分隔的观测数据对的个数 $,Z(x_i)$ 和 $Z(x_i+h)$ 为空间距离为,h 的点对的温度测定值。

图 1 和图 2 是水平方向(鼓风方向)和垂直方向(垂直鼓风方向)的半变异函数图。



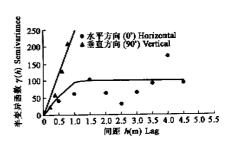


图 2 剖面 🛚 半变异函数图

Fig. 2 The semivariogram function of profile I

Fig. 1 石 表 表 表 figram function of profile I

在变异理论中,通常将空间相关的最大距离 $\alpha(\text{range})$ 称为极限距离。在图 1 和图 2 中,不同观测点的温度观测值之间的偏差,在一定的范围是一个随测点间距的增加而逐渐增大的过程,当测点间距 $h>\alpha$ 时,它们的方差趋于恒定。因此温度的实际观测值在堆体中分布不是完全随机的,在一定范围内,它们是隶属于空间轨迹的一种有序变化,只有在这一范围之外时,变化的轨迹方才消失,观测值之间的差异才具有均值为零、方差恒定的重要统计特性,才具备随机理论的应用条件。图 1 和图 2 还表明,在较为均一的水平方向,堆体中的温度变化是确定性变异和随机性变异共同作用的结果,确定性变化规律往往控制一定范围内温度的变化和分布。

水平方向(0°)的半变异函数可以用球函数模型进行拟合。

$$\begin{cases} \gamma(h) = C_0 + C \left[\frac{3}{2} \left(\frac{h}{a} \right) - \frac{1}{2} \left(\frac{h}{a} \right)^3 \right] (h < \alpha) \\ \gamma(h) = C_0 + C \end{cases}$$
 $(h \geqslant \alpha)$

拟合结果表明,当 h=0 时,块金方差 $C_0=0$,表明在最小取样距离之内由于温度变异性和测量误差所引起的方差为零。

剖面 $I \setminus I$ 的 α 值分别为 $0.90m \setminus 1.25m$ 。空间相关的最大距离 α 对于温度调查和统计分析中观测样点的设置具有重要的意义和参考价值。变程以内重复设置观测样点将是无效的,这样做违反了统计抽样的独立性原则,并且导致样本总方差的估计偏低 $I \setminus I$ 。

图 1 和图 2 表明,0°和 90°方向的半变异函数存在明显不同,这说明温度的空间变异是具有方向性的。温度在不同的方向上呈现不同的变异规律,各方向上的半变异函数曲线不会完全重合。鼓风作用和抽风效应是温度空间变异性存在方向性的主要原因[13]。

垂直方向(90°)的半变异函数可用线性模型进行拟合:

$$\begin{cases} \gamma(h) = C_0 + Ah & (h < a) \\ \gamma(h) = C_0 + C & (h \ge a) \end{cases}$$

当 h=0 时,块金方差 $C_0=0$ 。

剖面 I、I的变程分别为 0.75m、1.00m(图 2)。

综上所述,推体温度空间上的变化在一定范围内有着一定的相关关系,不能视为是完全独立的,半变异函数是分析温度空间关系的一种方法。用半变异函数研究堆肥温度在空间分布上的相关性,对于研究温度采样点之间的相关域,并依此来确定试验区域的大小和取样点的位置,从而达到样品之间完全独立具有重要意义。

2.2 堆体的剖面温度分析

在半变异分析的基础上,用克里格插值法对未测点的参数值进行最优内插估值。图 3 和图 4 为运用克里格插值法绘制的温度等值线图。



剖面长度 Length of profile(m)

图 3 剖面 I 的温度等值线分布 Fig. 3 The temperature isoline of profile I

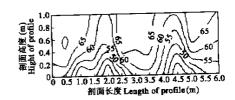


图 4 剖面 I 的温度等值线分布

Fig. 4 The temperature isoline of profile I

等值线间的平距越小,或等值线越密,则表示温度变异性越大。反之,平距越大,则表示温度变异性越小。从等值**药的税率据**可直观地判断温度在堆体中的不均匀性程度^[10]。

由于本堆肥系统堆肥池的风室较大,对于气流具有良好的缓冲作用,所以风量在风室中分布比较均

匀,而且布气板上的布气孔隙比例较大,整个堆体的供风量不是制约因素。图 3 和图 4 显示堆体中段出现的低温区与上堆操作方式有关。因为堆体规模较大,混料上堆时间分为两天,堆体中段在空气中暴露一段时间(12h),导致物料湿度减小,微生物活动减弱,堆体中段通气性也得到改善,堆体散热过程加快,因此堆体中段的温度较低。

剖面 I 对应 $0.79 \, \mathrm{m}^3/(\mathrm{min} \cdot \mathrm{m}^3)$ 的通风量,离池壁 $0.75 \, \mathrm{m}$,堆体的通风性能主要受混料比例的影响。图 3 显示, $0 \sim 2.0 \, \mathrm{m}$ 段基本没有低温区($\leq 50 \, \mathrm{C}$),低温区主要在 $2.0 \sim 6.0 \, \mathrm{m}$ 段的 $0 \sim 0.3 \, \mathrm{m}$ 层,没有达到处理要求的部分约为 7%。因为风向下端的风速快、风量大,堆体将会散失更多热量,因此可以根据风向下端堆体温度状况判断供风量的合适程度。图 3 表明,底层形成较长的低温区,表明供风量过大。

聂永丰等认为,强制通风静态垛堆肥系统的通风量经验值为 $0.05\sim0.2\text{m}^3/(\text{min}\cdot\text{m}^3)$ 。如果风量过大 (≥ $0.48\text{m}^3/(\text{min}\cdot\text{m}^3)$),大量热将通过水分蒸发而散失,使得堆温降得太低,不利于反应进行[14]。李艳霞等认为,强制通风静态垛的通风量经验值为 $0.06\text{m}^3/(\text{min}\cdot\text{m}^3)$ [15]。这些经验值的应用环境是堆肥系统采用"时间-温度"控制模式。本试验采用温度自动反馈控制模式,要求供氧快而充分,降温迅速,如果通风量太低,将无法达到工艺要求。控制系统使得堆体代表性位置的温度处于一个相对稳定的水平,设定的通风量能够起到控制温度的效果[11]。图 3 结果表明堆体底层温度过低,而且低温区域所占比例较大,说明风量需要调解。

Rusell 研究认为,对于自然通风静态垛堆肥系统,堆体的高温中心位于堆体上层 1/3 处,有时也位于堆体下层 1/3 处,有时也位于堆体 1/3 处,有时也位于推体 1/3 处,有时也位于推体 1/3 处,有时也位于推体 1/3 处,有时也有量 1/3 处,有量 1/3 处,有量 1/3 处,有量 1/3 处理,这种是 1/3 处理,是 1/3 处理,

剖面 \mathbb{I} 对应 $2.03\text{m}^3/(\text{min} \cdot \text{m}^3)$ 的通风量, $0\sim1.5\text{m}$ 基本没有低温区,低温区主要集中在 $3.5\sim6.0\text{m}$ 段的 $0\sim0.4\text{m}$ 层,约占总体积的 5%。通风量要求越高,所需风机的功率越大(或通风时间越长),从节能的角度出发,在不降低处理效果的前提下,减少通风量是堆肥工艺的改进优化方向之一。 试验的两种通风量都需要调整,因此中试规模堆肥的通风量应该在 $0.79\text{m}^3/(\text{min} \cdot \text{m}^3)$ 以下。

综上所述,利用克里格插值方法可以得到堆体温度等值线图。温度等值线图表明强制通风静态垛堆肥系统的堆体温度,从下至上形成梯度;堆体中段、下段的下层 $0\sim0.4m$ 温度相对较低,需要回流处理;高温中心一般出现于 0.4m 高度以上;中试规模堆肥的通风量应该调整,有待继续深入研究。

3 结论

本研究将地统计学理论引入堆肥科学,利用半变异函数分析堆肥温度的空间变异性。堆肥温度不仅着存在空间变异性,而且不同方向上的空间变异性还存在差异,水平方向的半变异函数用球模型模拟,垂直方向的半变异函数用线性模型模拟。两个剖面水平方向的变程分别为 0.90m、1.25m; 垂直方向的变程分别为 0.75m、1.00m。在进行半变异函数的分析的基础上,利用克里格插值方法进行最优内插估值。得到的温度等值线图表明,堆体高温中心一般在堆体中层 $0.4\sim0.6m$ 区域,低温区域一般在堆体下层 $0\sim0.4m$ 。从温度剖面等值线判断,中试规模堆体合理的通风量在 $0.79m^3/(min \cdot m^3)$ 以下。

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